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Transport Planning, Traffic Impact Assessments, Road Safety Audits, Expert Witness

14th October 2020 Reference: 200379.02FB

Lane Cove Council 48 Longueville Road Lane Cove

# LETTER OF RESPONSE REGARDING MIXED USE DEVELOPMENT AT 4 - 18 NORTHWOOD ROAD & 274 - 274A LONGUEVILLE ROAD, LANE COVE

### Greg

Reference is made to your request to provide supplementary information to assist Council in determining the development application for DA113/2020. The comments made by Council relevant to traffic and parking are outlined within Council's Traffic Engineers *Memorandum – Referral Request and Response* dated 23<sup>rd</sup> September 2020 and in an email dated 23<sup>rd</sup> September 2020 and 12<sup>th</sup> October 2020. A response has been provided to each of the comments made by Council (shown *italicised*), with the amended plans shown in **Annexure A** for reference.

A safety and functionality report for the traffic signals for the one-way ramp has been asked for

**MTE Response:** A queuing assessment has been undertaken to determine the queue impacts as a result of the single lane ramp. The following are relevant to note:

- The basement serving the single lane ramp will be restricted to staff parking only;
- It will be assumed to be conservative that all spaces will generate 1 vehicle trip in a single peak hour (highly conservative) resulting in a traffic generation of 44 vehicle trips
- The inbound and outbound distribution from the car park will follow that of typical office development being the following:
  - o AM peak hour period 90% inbound (40), 10% outbound (4);
  - o PM peak hour period 10% inbound (4), 90% outbound (40).

As noted above, staff development traffic is highly tidal as such to determine any sort of queuing that may occur due to the single lane ramp, the probability of a vehicle exiting the Level 1 Basement and entering the Level 1 Basement needs to be determined. Outside this conflict there is no conflict between opposing vehicle streams, such that there would be no vehicle queues.



To determine the conflict of opposing vehicle streams, reference is made to the Poisson Distribution as shown in **Figure 1** below. Which allows the determination of an event occurring over a given time interval or a specified region of space, which in our case is the time it would take a vehicle to travel along the one-way section of ramp.

The **probability distribution of a Poisson random variable** X representing the number of successes occurring in a given time interval or a specified region of space is given by the formula:

$$P(X) = \frac{e^{-\mu}\mu^x}{x!}$$

where

 $x = 0, 1, 2, 3 \dots$ 

e = 2.71828 (but use your calculator's e button)

 $\mu =$  mean number of successes in the given time interval or region of space

#### FIGURE 1: POISSON DISTRIBUTION

The above determination of conflict between opposing vehicle streams has been undertaken based upon the following considerations:

- A distance of 50m between passing opportunities (i.e. the distance where access is restricted to one vehicle);
- Based upon the 50m and a travel speed of 5km/h (highly conservative), the resulting time it takes to travel the 50m distance is 36 seconds;
- Adopting an addition factor of safety of 4 seconds for the light to turn from red to green or vice versa results in a travel time of 40 seconds;
- Inbound traffic of 40 vehicle trips;
- Outbound traffic of 4 vehicle trips.

Adopting the above time of conflict, vehicle trips and direction, the probability of conflict along the 50m length of assessed area is 3.52%. As shown, this is a low chance of conflict between vehicle streams, resulting in one conflict occurring every 28 AM peak hour period. When that conflict does occur, 92% of the time there would only be one vehicle waiting or 8% of the time there would be more than one vehicle waiting for the inbound traffic stream (40 vehicle trips). It should be noted that the 99<sup>th</sup> percentile queue is two (2) vehicles.

The above would also be the same during the PM peak hour period, but in the reverse direction, i.e. 4 inbound vehicle trips and 40 outbound (98<sup>th</sup> percentile queue of 2 vehicles when event occurs) vehicle trips.

Overall, the probability of the event occurring is low and the likelihood that there would be two (2) vehicles waiting due to the event would also be extremely rare. Considering this, the operation of the signals is deemed safe which will not have an adverse impact to other users of the car park.

It is recommended that *AGD Systems* be approached to provide a functionality report, which is in the process of occurring which will be provided to Council when available. It is expected that priority to entering vehicles will occur, that is the signal will show a green light on parking Level 2 and a red



light on parking Level 1 and will only change once a vehicle is waiting within the loading bay on parking Level 1.

The upgrade to the River Road / Longueville Road intersection needs to be reflected in their traffic model.

**MTE Response:** Modifications have been undertaken to the SIDRA model to reflect the upgraded conditions, specifically the following:

- Removal of the left turn left (high angle) slip lane from River Road West into Longueville Road:
- Addition of a right turn lane from Longueville Road into River Road West;
- Pedestrian signal control over the full length of the approach to the signalised intersection from Longueville Road.

It is relevant to note that the right turn volume from Longueville Road has been left as a single vehicle (1), as this is a new vehicle movement from existing conditions and it is not known the displaced traffic volume that will use this movement compared to existing observed traffic.

The updated SIDRA model is shown in **Table 1** below, with detailed SIDRA outputs reproduced in **Annexure B** for reference. The implemented TCS plan has also been modified to reflect that as shown in **Annexure C** for reference.

It should be noted that both existing and future scenarios have the upgraded road geometry.



### **TABLE 1: INTERSECTION PERFORMANCE (SIDRA INTERSECTION 9.0)**

			Average Delay <sup>(2)</sup>	•								
Intersection	Peak Hour	Degree of Saturation <sup>(1)</sup>	(sec/veh)	Level of Service <sup>(3)(4)</sup>	Control Type	Worst Movement						
EXISTING PERFORMANCE – WITH FUTURE ROAD GEOMETRY												
Longueville Road / Northwood Road /	АМ	0.73	17.4	В	Signals	RT from Longueville Road						
River Road West	PM	0.60	8.6	А		RT from Longueville Road						
Kenneth Street / Northwood Road	АМ	0.45	9.4	Α	Signals	RT from Kenneth Street						
Northwood Road	PM	0.64	13.2	А		RT from Kenneth Street						
		FUTURE PERI	FORMANCE – WITH FU	TURE ROAD GEO	METRY							
Longueville Road / Northwood Road /	АМ	0.73	17.4	В	Signals	RT from Longueville Road						
River Road West	PM	0.62	8.7	А		RT from Longueville Road						
Kenneth Street /	AM	0.44	9.5	Α	Signals	RT from Kenneth Street						
Northwood Road	PM	0.65	13.7	В	· •	RT from Kenneth Street						

#### NOTES:

As shown above, the assessed signalised intersections of Kenneth Street / Northwood Road and Longueville Road / Northwood Road / River Road West retain an existing Level of Service of "A" or "B" during the both AM and PM peak hour periods. This indicates acceptable delays and additional spare capacity maintained. As such it can be concluded that the proposed development will not have an adverse impact upon the operation of the assessed signalised intersection under future road geometry conditions.

<sup>(1)</sup> The Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.

<sup>(2)</sup> The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.

<sup>(3)</sup> The Level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from A to F, with A representing the best operational condition and level of service F the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.

<sup>(4)</sup> No overall Level of Service is provided for Give Way and Stop controlled intersections as the low delays associated with the dominant movements skew the average delay of the intersection. The Level of Service of the worst approach is an indicator of the operation of the intersection, with a worse Level of Service corresponding to long delays and reduced safety outcomes for that approach.



The development provides two accessible parking spaces where one space is not in accordance with the standard. The development is required to provide a total of 86 parking spaces including 3 accessible parking spaces. The accessible parking spaces are to be in accordance with AS2890.6.

The accessible parking spaces are required to be located as close to the lift as possible;

**MTE Response:** The disabled car parking provision has been provided based upon the requirements within the Building Code of Australia over Council's DCP requirements. In any event the plans have been amended to reflect the provision of three (3) disabled car parking spaces for the development, which have been relocated close to the lifts.

Access in/out of spaces 18 and 19 require vehicles to reverse onto the circular ramp with limited visibility. As such, these spaces are to be deleted.

**MTE Response:** The circular portion on Level 2 is flat, as the ramp ends further to the south, such that there are unrestricted sight lines to both of these spaces for vehicles travelling along the ramp. If still preferred by Council these spaces can be removed.

All parking spaces are to be line marked according to their relevant component.

**MTE Response:** Car parking spaces will be linemarked and constructed in accordance with the relevant Australian Standard requirements. To ensure this occurs it is recommended that it be conditioned. The allocation of car parking will be the following:

- 3 x set down / pick-up spaces on Level 3 Allocated to no one and can be used by emergency facilities;
- 10 x residential aged care facility visitor spaces on Level 3;
- 4 x residential aged care facility visitor spaces on Level 2;
- 28 x commercial visitor spaces on Level 2;
- 20 x residential staff aged care facility on Level 1;
- 24 x commercial staff aged care facility on Level 1.

The above provision complies with Council's DCP and the SEPP (Affordable Rental Housing)

Driveway to be designed as left in and left out only. The design should prevent right turn movements by installing a triangular median Island at the entry/exit of the driveway. Detail of the driveway showing this restriction is to be provided;

**MTE Response:** This type of design can be accommodated, but in the first instance the preference would be to restrict vehicle movements into and out of the site via a raised median located within Northwood Road, subject to approval by Council's Local Traffic Committee.

AutoCAD files of the ground clearance test is to be provided for a B99 and MRV as the plan provided is unclear;

MTE Response: Autocad files will be provided showing ground clearance testing.

It is noted that the height clearance provided is not in accordance with AS2890.2. Ramp sections are to be provided indicating the height clearance for the largest design vehicles accessing the development;



**MTE Response:** Long sections are provided within **Annexure A**, indicating a headroom of 3.6m for the entry driveway ramp, 2.6m headroom for the ramp between Level 3 and Level 2 and a headroom of 2.2m for the ramp between Level 2 and Level 1.

The traffic report must consider the following future upgrade projects:

River Road/Longueville Road upgrade – Modelling is required to be updated as per the TCS provided;

Northwood Roundabout – Council is the process of gaining approval for a roundabout at the Northwood Road/River Road intersection. Given the development is restricted to left in/left out access, the proposed roundabout will facilitate westbound movements from the development which will potentially reduce rat-running through local streets. As such, the developer is required to contribute funding towards the construction of the proposed roundabout.

**MTE Response:** The modelling has been amended and is reflected in a previous response. In regard to contributing funds, this is for others to address.

The use of traffic counts to determine the traffic generation of the existing development (as oppose to rates from the RMS Guide) would be an accurate representation of existing conditions and therefore the net increase in traffic volumes. Passing trade of 80% should be applied to the service station and convenience store component of the existing development

**MTE Response:** The RMS Guide to Traffic Generating Developments is an accepted methodology to determine traffic generation of various land uses and is an appropriate method to estimate the existing and future traffic generation of the site.

At the time the traffic report was prepared, some of the shops at the existing site were not occupied. Hence, it was not possible to accurately capture existing traffic generation of the site through the use of surveys. If further investigation is required into existing development traffic generation, it is recommended that the traffic reports for the existing sites be reviewed to determine the approved traffic generation of the existing sites.

Further, the car parking layouts of the existing sites and access arrangements would likely play a role in development traffic associated with the development, such that the use of surveys to capture existing development traffic is not an appropriate method. That is there is potential that the traffic generation of the existing sites do not all occur at the existing site driveways, but also within the surrounding road network, i.e. visitors to the existing sites may park elsewhere and not solely restricted to on-site.

The traffic assessment and modelling undertaken to date does not remove any existing traffic generated from the existing development, but rather adds the full proposed development traffic generation of the site. This provides a conservative assessment. In regards to passing trade, there is no evidence to suggest that passing trade for service stations is 80%.



Please contact the undersigned on 8355 2440 should you require further information or assistance. Yours faithfully,

M<sup>c</sup>Laren Traffic Engineering

Matthew M<sup>c</sup>Carthy
Senior Traffic Engineer
BE Civil Engineering
Masters of Engineering Science
RMS Accredited Level 1 Road Safety Auditor





## ANNEXURE A: AMENDED PLANS (Sheet 1 of 5)





## ANNEXURE A: AMENDED PLANS (Sheet 2 of 5)





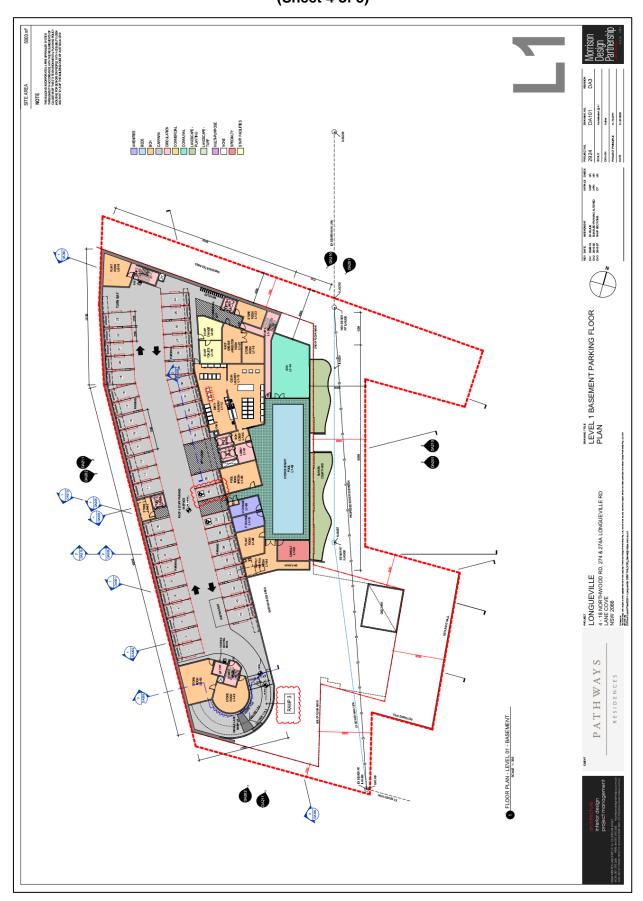
### ANNEXURE A: AMENDED PLANS

(Sheet 3 of 5)





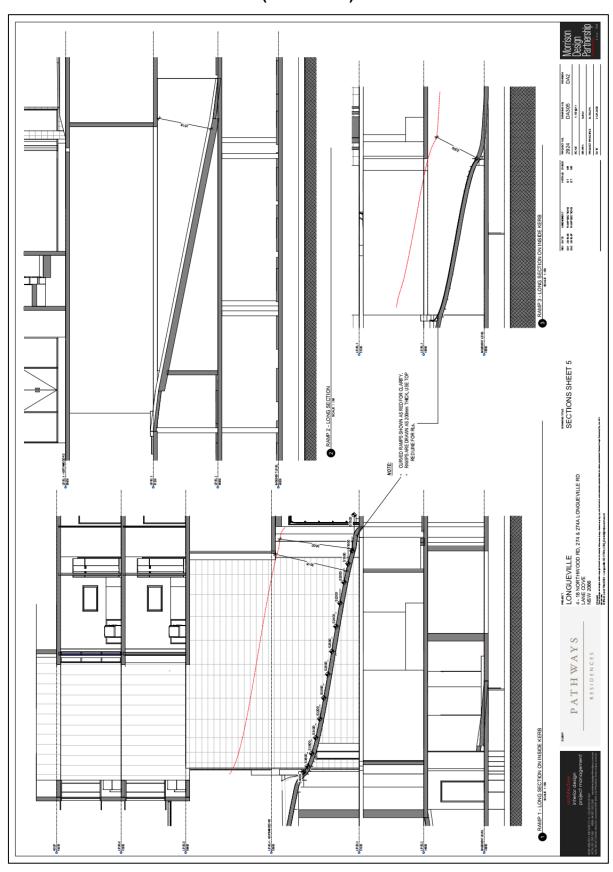
## ANNEXURE A: AMENDED PLANS (Sheet 4 of 5)





### ANNEXURE A: AMENDED PLANS

(Sheet 5 of 5)





## ANNEXURE B: SIDRA RESULTS (Sheet 1 of 4)

### CCG MOVEMENT SUMMARY

■ Network: N101 [EX AM Signals (Network Folder:

□□ Common Control Group: CCG1

General)]

[1]

Lil														
EQUI	SAT (Fi	xed-Tim	e/SCA	TS) Isol	ated C	ycle Tin	ne = 70	seconds	(CCG O	ptimum C	Cycle Tir	me - Minimເ	ım Delay)	
Vehic	le Mov	ement F	Perfori	mance (	CCG)									
Mov		DEMA		ARRI		Deg.	Δver	Level of		ACK OF	Prop.	Effective	Aver. No.	Aver.
ID	Turn	FLO\		FLOV		Satn	Delay	Service		IEUE	Que	Stop Rate	Cycles	
		[ Total	HV]		HV]	21/0			[ Veh.	Dist ]				· ·
0:1: 4	04 54 84	veh/h	%	veh/h	%	v/c	sec	(1	veh	m				km/h
	_		-	ille / Nort	nwood	i / River i	Road W	estj						
		ood Roa												
1a	L1	519	0.0	519	0.0	0.388	4.7	LOS A	3.4	23.6	0.21	0.58	0.21	50.0
2	T1	254	0.0	254	0.0	* 0.609	24.0	LOS B	8.2	57.1	1.00	0.90	1.00	34.7
Approa	ach	773	0.0	773	0.0	0.609	11.0	LOS A	8.2	57.1	0.47	0.69	0.47	43.7
North:	Longue	ville Roa	ıd											
8	T1	183	0.0	183	0.0	0.438	19.8	LOS B	5.0	35.1	0.82	0.69	0.82	36.4
9b	R3	1	0.0	1	0.0	0.005	35.3	LOS C	0.0	0.2	0.89	0.60	0.89	37.2
Approa	ach	184	0.0	184	0.0	0.438	19.9	LOS B	5.0	35.1	0.82	0.69	0.82	36.5
North\	Nest Ri	ver Road	t West											
27b	L3	163	0.0	163	0.0	0.731	23.5	LOS B	13.1	91.6	0.82	0.86	0.88	43.3
29a	R1	977	0.0	977	0.0	*	20.9	LOS B	18.9	132.5	0.85	0.86	0.88	35.6
Approa	ach	1140	0.0	1140	0.0	0.731	21.3	LOS B	18.9	132.5	0.84	0.86	0.88	37.2
All Vel	nicles	2097	0.0	2097	0.0	0.731	17.4	LOS B	18.9	132.5	0.70	0.78	0.72	39.2
Site: 1	01 [AM	- EX - No	orthwo	od / Kenr	neth]									
South	East: No	rthwood	Road											
21	L2	16	0.0	16	0.0	0.445	18.5	LOS B	9.5	66.2	0.70	0.62	0.70	48.4
22	T1	616	0.0	616	0.0	0.445	12.9	LOS A	9.5	66.2	0.70	0.61	0.70	42.2
Approa	ach	632	0.0	632	0.0	0.445	13.0	LOS A	9.5	66.2	0.70	0.61	0.70	42.5
NorthF	ast Pe	trol Station	on Acc	ess										
24	L2	17	0.0	17	0.0	0.029	7.6	LOS A	0.1	1.0	0.32	0.62	0.32	52.0
26	R2	1	0.0	1	0.0	0.029	7.7	LOS A	0.1	1.0	0.32	0.62	0.32	48.0
Approa		18	0.0	18	0.0	0.029	7.6	LOS A	0.1	1.0	0.32	0.62	0.32	51.8
North	Nest: No	orthwood	l Road											
27	L2	15	0.0	15	0.0	0.381	8.1	LOS A	7.1	49.9	0.44	0.40	0.44	50.0
28	T1	1024	0.0	1024	0.0	0.381	3.0	LOS A	7.1	49.9	0.28	0.25	0.28	54.9
29	R2	117	0.0	117	0.0	*	6.0	LOS A	0.7	4.7	0.29	0.61	0.29	48.6
Approa		1156	0.0	1156	0.0	0.208	3.4	LOS A	7.1	49.9	0.28	0.29	0.28	54.1
		enneth S												
30	L2	158	0.0	158	0.0	0.248	23.5	LOS B	3.9	27.4	0.76	0.76	0.76	34.1
32	R2	87	0.0	87	0.0	0.366	37.2	LOS C	2.9	20.2	0.95	0.76	0.95	36.6
Approa		245	0.0	245	0.0	0.366	28.4	LOS B	3.9	27.4	0.83	0.76	0.83	35.3
All Vel	nicles	2051	0.0	2051	0.0	0.445	9.4	LOS A	9.5	66.2	0.48	0.45	0.48	46.8



## ANNEXURE B: SIDRA RESULTS (Sheet 2 of 4)

### CCG MOVEMENT SUMMARY

Common Control Group: CCG1 Network: N101 [EX PM Signals (Network Folder: General)]

[1]														
EQUIS	SAT (Fix	xed-Time	e/SCAT	ΓS) Isola	ted Cy	cle Time	= 72 se	conds (C	CCG Opt	imum Cy	cle Tim	e - Minimum	n Delay)	
Vehic	le Move	ement P	erform	ance (C	CG)									
Mov		DEMA		ARRI'		Deg.	Aver.	Level of		ACK OF	Prop.	Effective A	ver. No.	Aver.
ID	Turn	FLO\		FLO\		Satn		Service		EUE		Stop Rate	Cycles	
		[ Total veh/h	HV ] %	[ Total veh/h	HV ] %	v/c	sec		[ Veh. veh	Dist ] m				km/h
Site: 10	11 [PM .					' River Roa		f]	Veii	- '''	_			KIII/II
	-	ood Road	•	ic / Ivorui	wood /	TOTAL TOTAL	au 7703	·]						
1a	L1	1131	0.0	1131	0.0	0.600	3.4	LOS A	2.9	20.1	0.11	0.50	0.11	52.1
						*								
2	T1	209	0.0	209	0.0	0.600	0.9	LOS A	1.8	12.8	0.11	0.37	0.11	55.9
Approa	ach	1340	0.0	1340	0.0	0.600	3.0	LOS A	2.9	20.1	0.11	0.48	0.11	52.7
North:	Longue	ville Road	d											
8	T1	253	0.0	253	0.0	0.463	20.8	LOS B	7.2	50.1	0.84	0.71	0.84	35.8
9b	R3	1	0.0	1	0.0	0.005	36.4	LOS C	0.0	0.2	0.89	0.60	0.89	36.8
Approa	ach	254	0.0	254	0.0	0.463	20.9	LOS B	7.2	50.1	0.84	0.71	0.84	35.8
NorthV	Vest: Riv	ver Road	West											
27b	L3	74	0.0	74	0.0	0.328	18.0	LOS B	5.5	38.3	0.63	0.75	0.63	46.4
29a	R1	503	0.0	503	0.0	0.328	16.1	LOS B	6.6	46.2	0.63	0.75	0.63	39.2
Approa	ach	577	0.0	577	0.0	0.328	16.3	LOS B	6.6	46.2	0.63	0.75	0.63	40.6
All Veh	icles	2171	0.0	2171	0.0	0.600	8.6	LOS A	7.2	50.1	0.33	0.57	0.33	46.4
Site: 10	01 [PM -	- EX - No	rthwoo	d / Kenne	eth]									
SouthE	ast: No	rthwood	Road											
21	L2	31	0.0	31	0.0	0.635	20.0	LOS B	16.0	111.7	0.79	0.71	0.79	47.4
22	T1	1206	0.0	1206	0.0	*	14.3	LOS A	16.0	112.0	0.79	0.71	0.79	41.0
Approa	nch	1237	0.0	1237	0.0	0.635 0.635	14.4	LOS A	16.0	112.0	0.79	0.71	0.79	41.2
					0.0	0.000		2007	10.0	112.0	0.70	0.7 1	0.70	71.2
		rol Statio												
24	L2	16	0.0	16	0.0	0.025	8.8	LOS A	0.1	0.9	0.42	0.64	0.42	51.2
26	R2	2 18	0.0	2 18	0.0	0.025	8.8	LOS A	0.1	0.9	0.42	0.64	0.42	46.7
Approa	ICH	10	0.0	10	0.0	0.025	0.0	LOS A	0.1	0.9	0.42	0.64	0.42	50.9
NorthV	Vest: No	rthwood	Road											
27	L2	14	0.0	14	0.0	0.214		LOS A	5.6	39.5	0.60	0.53	0.60	48.0
28	T1	577	0.0	577	0.0	0.214	4.7	LOS A	5.6	39.5	0.43	0.38	0.43	52.4
29	R2	160	0.0	160	0.0	* 0.392	14.0	LOS A	3.0	20.8	0.90	0.80	0.90	40.6
Approa	ach	751	0.0	751	0.0	0.392	6.8	LOS A	5.6	39.5	0.53	0.47	0.53	49.3
SouthV	Vest: Ke	enneth St	reet											
30	L2	133	0.0	133	0.0	0.214	24.3	LOS B	3.4	23.7	0.76	0.75	0.76	33.6
32	R2	75	0.0	75	0.0	0.322	38.1		2.5	17.7	0.95	0.76	0.95	36.3
Approa	ach	207	0.0	207	0.0	0.322	29.3	LOS C	3.4	23.7	0.83	0.75	0.83	35.0
All Veh	icles	2213	0.0	2213	0.0	0.635	13.2	LOS A	16.0	112.0	0.70	0.63	0.70	42.8



### ANNEXURE B: SIDRA RESULTS (Sheet 3 of 4)

### CCG MOVEMENT SUMMARY

L2

R2

158

98

256

2074

0.0

0.0

0.0

0.0

158

98

256

2074

0.0

0.0

0.0

0.0

30

32

Approach

All Vehicles

Network: N101 [FU AM Signals (Network Folder: General)]

□□ Common Control Group: CCG1
[1]

General

1.1														
EQUI	SAT (Fi	xed-Tim	e/SCA	TS) Isol	ated C	ycle Tin	ne = 72	seconds	(CCG C	Optimum (	Cycle Tir	ne - Minimi	um Delay)	
Vehic	le Mov	ement F	Perforr											
Mov ID	Turn	DEMA FLO\ [ Total veh/h		ARRI\ FLO\ [ Total veh/h		Deg. Satn v/c	Aver. Delay sec	Level of Service		ACK OF JEUE Dist ] m	Prop. Que	Effective Stop Rate	Aver. No. Cycles	
Site: 1	01 [AM	- FU - Lo						est1	VEII	- '''				KIII/II
	-	ood Roa	•			,		,						
1a	L1	527	0.0	527	0.0	0.389	4.6	LOS A	3.4	24.0	0.20	0.58	0.20	50.1
2	T1	258	0.0	258	0.0	* 0.631	25.3	LOS C	8.2	57.1	1.00	0.92	1.01	33.9
Appro	ach	785	0.0	785	0.0	0.631	11.4	LOS B	8.2	57.1	0.46	0.69	0.47	43.3
North:	Longue	ville Roa	ad											
8 9b	T1 R3	186 1	0.0	186 1	0.0	0.480 0.005	21.3 36.4	LOS C LOS D	5.4 0.0	37.8 0.2	0.84 0.89	0.71 0.60	0.84 0.89	35.4 36.8
Appro		187	0.0	187	0.0	0.480	21.4	LOS C	5.4	37.8	0.84	0.71	0.84	
North	West: Ri	ver Road	d West											
27b	L3	163	0.0	163	0.0	0.729	23.2	LOS C	13.1	91.6	0.81	0.86	0.87	43.5
29a	R1	991	0.0	991	0.0	* 0.729	20.4	LOS C	19.5	136.4	0.84	0.85	0.86	
Appro	ach	1154	0.0	1154	0.0	0.729	20.8	LOS C	19.5	136.4	0.83	0.85	0.86	37.5
All Ve	hicles	2126	0.0	2126	0.0	0.729	17.4	LOS B	19.5	136.4	0.70	0.78	0.71	39.2
Site: 1	01 [AM	- FU - N	orthwo	od / Keni	neth]									
South	East: No	orthwood	Road											
21 22	L2 T1	16 629	0.0	16 629	0.0	0.442 0.442	18.2 12.6	LOS B LOS B	9.7 9.7	67.9 67.9	0.69 0.69	0.61 0.60	0.69 0.69	48.6 42.5
Appro	ach	645	0.0	645	0.0	0.442	12.7	LOS B	9.7	67.9	0.69	0.60	0.69	
North\	West: No	orthwood	Road											
28	T1	1056	0.0	1056	0.0	0.382	2.9	LOS A	7.4	51.5	0.27	0.24	0.27	55.2
29	R2	117	0.0	117	0.0	* 0.209	7.0	LOS A	0.8	5.3	0.33	0.63	0.33	
Appro	ach	1173	0.0	1173	0.0	0.382	3.3	LOS A	7.4	51.5	0.28	0.28	0.28	54.4
South	West: K	enneth S	Street											

0.255

0.422

0.422

0.442

24.6

38.7

30.0

9.5

LOS C

LOS D

LOS C

LOS A

4.1

3.4

4.1

9.7

28.6

23.5

28.6

67.9

0.77

0.97

0.84

0.48

0.76

0.77

0.76

0.44

0.77

0.97

0.84

0.48

33.4

36.1

34.8

46.6



## ANNEXURE B: SIDRA RESULTS (Sheet 4 of 4)

### CCG MOVEMENT SUMMARY

Common Control Group: CCG1 Network: N101 [FU PM Signals (Network Folder: General)]

EQUIS	SAT (Fix	ked-Time	e/SCAT	S) Isola	ted Cyc	ele Time :	= 72 se	conds (C	CCG Opt	imum Cy	cle Time	e - Minimun	n Delay)	
Vehic	le Move	ement P	erform	ance (C	CG)									
Mov	_	DEMA		ARRI'		Deg.	Aver.	Level of		ACK OF	Prop.	Effective A	Aver. No.	Aver.
ID	Turn	FLO\ [ Total	ws HV]	FLO\ [Total	ws HV]			Service	Veh.	EUE Dist ]		Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh.	m m				km/h
Site: 1	01 [PM -					River Roa		t]						
South:	Northwo	ood Road	d											
1a	L1	1156	0.0	1156	0.0	0.616	3.4	LOS A	3.0	21.0	0.11	0.50	0.11	52.1
2	T1	215	0.0	215	0.0	* 0.616	0.9	LOS A	1.9	13.2	0.12	0.37	0.12	56.0
Approa	ach	1371	0.0	1371	0.0	0.616	3.0	LOS A	3.0	21.0	0.11	0.48	0.11	52.7
North:	Longue	ville Road	d											
8	T1	259	0.0	259	0.0	0.487	21.1	LOS C	7.4	51.9	0.85	0.71	0.85	35.6
9b	R3	1	0.0	1	0.0	0.005	36.4	LOS D	0.0	0.2	0.89	0.60	0.89	36.8
Approa	ach	260	0.0	260	0.0	0.487	21.1	LOS C	7.4	51.9	0.85	0.71	0.85	35.6
NorthV	Vest: Riv	er Road	West											
27b	L3	74	0.0	74	0.0	0.339	18.0	LOS B	5.6	39.1	0.63	0.75	0.63	46.4
29a	R1	517	0.0	517	0.0	0.339	16.2	LOS B	6.9	48.0	0.64	0.75	0.64	39.1
Approa	ach	591	0.0	591	0.0	0.339	16.4	LOS B	6.9	48.0	0.64	0.75	0.64	40.5
All Veh	nicles	2221	0.0	2221	0.0	0.616	8.7	LOS A	7.4	51.9	0.34	0.58	0.34	46.4
Site: 1	01 [PM -	FU - No	rthwoo	d / Kenne	eth]									
South	East: No	rthwood	Road											
21	L2	31	0.0	31	0.0	0.651	20.2	LOS C	16.6	115.9	0.80	0.72	0.80	47.3
22	T1	1237	0.0	1237	0.0	* 0.651	14.4	LOS B	16.6	116.1	0.80	0.71	0.80	40.8
Approa	ach	1267	0.0	1267	0.0	0.651	14.6	LOS B	16.6	116.1	0.80	0.71	0.80	41.1
NorthV	Vest: No	rthwood	Road											
28	T1	613	0.0	613	0.0	0.222	4.5	LOS A	5.8	40.5	0.42	0.37	0.42	52.8
29	R2	160	0.0	160	0.0	* 0.397	14.5	LOS B	3.1	21.5	0.91	0.80	0.91	40.3
Approa	ach	773	0.0	773	0.0	0.397	6.6	LOS A	5.8	40.5	0.53	0.46	0.53	49.6
South\	Nest: Ke	enneth St	reet											
30	L2	133	0.0	133	0.0	0.214	-	LOS C	3.4	23.7	0.76	0.75	0.76	33.6
32	R2	121	0.0	121	0.0	0.521		LOS D	4.2	29.5	0.98	0.78	0.98	35.9
Approa	ach	254	0.0	254	0.0	0.521	31.4	LOS C	4.2	29.5	0.86	0.77	0.86	35.1
All Vel	nicles	2294	0.0	2294	0.0	0.651	13.7	LOS B	16.6	116.1	0.71	0.63	0.71	42.4



### ANNEXURE C: TCS PLAN AS PROVIDED BY COUNCIL

